Modified Level II Streambed-Scour Analysis for Structure I-69-76-4775 Crossing Salamonie River in Huntington County, Indiana

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Prepared in cooperation with the INDIANA DEPARTMENT OF TRANSPORTATION

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CONVERSION FACTORS AND ABBREVIATIONS

Multiply	Ву	To obtain
inch (in.)	25.4	millimeter
foot (ft)	0.3048	meter
square foot (ft²)	929.0	square centimeter
feet per second (ft/s)	0.3048	meters per second
cubic foot per second (ft ³ /s)	0.02832	cubic meter per second
mile (mi)	1.609	kilometer
square mile (mi ²)	2.590	square kilometer

Abbreviations used in this report:

D_{50}	median diameter of bed material
Q100	100-year discharge
FEMA	Federal Emergency Management Agency
HEC	Hydraulic Engineering Circular
IDNR	Indiana Department of Natural Resources
INDOT	Indiana Department of Transportation
USGS	U. S. Geological Survey
WSPRO	Water Surface PROfile model

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ABSTRACT

Level II scour evaluations follow a process in which hydrologic, hydraulic, and sediment-transport data are evaluated to calculate the depth of scour that may result when a given discharge is routed through a bridge opening. The results of the modified Level II analysis for structure I-69-76-4775 on Interstate 69 crossing Salamonie River in Huntington County, Indiana, are presented. The site is near the town of Warren in the southeastern part of Huntington County. Scour depths were computed with the Water Surface PROfile model, version V050196, which incorporates the scour-calculation procedures outlined in Hydraulic Engineering Circular No. 18. Total scour depths at the piers were approximately 13.7 feet for the modeled discharge of 15,800 cubic feet per second and approximately 20.9 feet for the modeled discharge of 26,900 cubic feet per second.

INTRODUCTION

The U.S. Geological Survey (USGS), in cooperation with the Indiana Department of Transportation (INDOT), is conducting Level II scour analyses at a number of bridges throughout Indiana. This report describes the methods applied and the modeling results for bridge I-69-76-4775.

Background and Scope

Level I scour assessment is a process where a large number of bridges are studied as a group. Assessments usually are made by evaluating a combination of geomorphic, hydrologic, and bridge-characteristic data. The results help investigators determine which bridges appear to be most likely to experience streambed-scour problems and which bridges appear to be relatively immune to problems brought on by streambed scour (for example, bridges built on bedrock).

When applied correctly, Level I scour assessments provide an investigator with information to identify those bridges that appear to be relatively safe and those bridges that fall into higher risk categories.

Level II scour evaluations describe the process for an investigator to apply a model to a bridge site and calculate the potential depth of scour that may result from a given flood event. Level II analyses involve the application of basic hydrologic, hydraulic, and sediment-transport engineering concepts and may include an evaluation of flood history, channel hydraulic conditions (for example, water-surface profile analysis), and basic sediment-transport analyses such as scour calculations (Lagasse and others, 1995).

The methods and model outlined in Hydraulic Engineering Circular (HEC) No. 18 (Richardson and Davis, 1995) formulate the basis for Level II scour evaluations. Methods used in this study for Level II scour evaluations are a modification of the HEC-18 standards. These modifications were made to comply with the methodology requested by INDOT (Merril Dougherty, Indiana Department of Transportation, oral commun., 1996). Descriptions of the specific modifications are given in the "Evaluation Methods" section of this report.

This report presents the methods followed for modeling, special considerations for this study site, and the input for and the output from the Water Surface PROfile (WSPRO) model.

Site Description

The study site is located near the town of Warren in the southeastern part of Huntington County. The drainage area for the site is approximately 412 mi² (estimated using Hoggatt, 1975, and USGS 7.5-minute topographic data). The predominant land use in the basin is agricultural; in the immediate vicinity of the bridge, the land is predominantly forest with some pasture land nearby.

Within the immediate vicinity of the bridge, Salamonie River has a channel-bed slope of approximately 0.0004 ft/ft. The channel-bed material is gravelly sand, and the channel banks consist of sandy silt-clay. At the time of the Level I site visit on June 23, 1993, the banks were observed to have 0 to 25 percent woody vegetative cover; the field report noted that the banks were experiencing fluvial erosion.

The Interstate 69 crossing of Salamonie River is a 413-ft-long, multi-lane bridge consisting of six spans supported by concrete and steel piers and sloping concrete spill-through abutments. Additional details describing conditions at the site are included in the Level I data base (Hopkins and Robinson, unpub. data, 1997). Photographs of the site, taken at the time of the Level I site visit, are archived at the USGS office in Indianapolis.

EVALUATION METHODS

The methods described in this section apply to a number of bridge sites in Indiana being evaluated for scour and outline the procedures requested by INDOT for these modified Level II scour analyses. The principal modification requested by INDOT was that the input data to the model come from or be estimated from existing data sources; no additional field data were collected. Actual methods used in the scour evaluation at this particular bridge site use the most applicable method possible, given the data available.

To determine drainage area, either published values found in Hoggatt (1975) or 7.5-minute topographic maps with Hoggatt's original drainage-area delineations were used. Where there are no published data, drainage-area segments measured from the maps produced by Hoggatt were either subtracted from downstream sites or added to upstream sites published by Hoggatt (1975).

In Indiana, flood discharges are coordinated by agreement among State and Federal agencies. At sites where flood discharges officially are coordinated among State and Federal agencies in Indiana, the coordinated 100-year discharge (Q100) was modeled. INDOT also provided an additional flood discharge for these coordinated sites in excess of the Q100 to be modeled.

If a flood discharge was not coordinated, the USGS examined Federal Emergency Management Agency (FEMA) studies for Q100 determinations. Where FEMA studies did not produce a Q100, the USGS contacted IDNR for an estimated Q100 in the vicinity of the site being studied. If IDNR did not have a O100, data from nearby USGS streamflow-gaging stations were analyzed with nearby and similar drainage basins that have been coordinated. At sites having no coordinated discharge data, the two discharges used in the model were 1) the approximated O100 and 2) a discharge equal to 1.7 times the approximated O100.

Most of the cross-section and bridge-opening geometry data were taken from the bridge plans (Indiana State Highway Commission, 1962) provided by INDOT. Bridge plans are presumed to be representative of current conditions at the site. To determine the cross-section geometry, a line was drawn on the bridge plans parallel to the bridge stationing and approximately one bridge width from the bridge. For sites where the bridge plans did not extend far enough laterally for collection of all cross-section data required for WSPRO model analysis, additional data were collected from 7.5-minute topographic maps.

The roadway and embankment profile was taken from the bridge and highway plans for those sites where roadway overtopping was expected. The INDOT bridge plans and 7.5-minute topographic maps were used as a guide, based on the water-surface elevations calculated by the WSPRO model, to determine if roadway overtopping might occur.

Roughness values (*n*-values) for the main channel were estimated by viewing photographs archived from the Level I scour assessments. The *n*-values for the overbanks were assigned on the basis of the surface-cover data summarized in the Level I data base (Hopkins and Robinson, unpub. data, 1997). From those data, the following roughness values were assigned to the surface-cover categories: urban—0.050, suburban—0.035, row crop—0.045, pasture—0.035, brush—0.120, forest—0.100, and wetland (any area covered by standing water)—0.100. The *n*-values for the overbanks were adjusted if the Level I photographs provided sufficient detail to warrant an adjustment.

WSPRO version V050196 was used to model flow through the study site. Starting watersurface elevation was obtained with a slope-conveyance computation. The channel-bed slope in the immediate vicinity of the bridge was estimated from the 7.5-minute topographic map and was used as the slope of the energy grade line for this computation.

WSPRO version V050196 includes a field that allows the input of up to four scour-adjustment factors (K1 to K4). For this modeling, the default value for K4 (bed armoring) was chosen. For scour-adjustment factors K1 and K2 (pier-nose shape and angle of attack, respectively), input values were determined by evaluating the data archived in the Level I data base (Hopkins and Robinson, unpub. data, 1997). For the K3 factor (bed forms), a value of 1.1 was applied in all cases.

In some cases, piers set on the overbanks are constructed with footings that are higher in elevation than pier footings in the main channel. In these situations, if the channel position changes, the piers that were initially constructed on the overbank may become part of the main channel. Therefore, to evaluate total potential scour, the model results obtained for contraction scour and deepest local scour in the main channel were added and applied to all piers in the bridge opening. This methodology allowed for an evaluation of potential undermining of pier supports in the event that future channel movement placed overbank piers in the main channel.

Where bridge pairs have a continuous abutment or fill between the bridges that does not allow expansion of flow, the bridge pair was modeled as one bridge. Sites with discontinuous abutments, allowing expansion between the bridges, were modeled as two separate bridges. In those cases, a valley cross section was measured between the bridges and used as the approach section for the downstream bridge and as the exit section for the upstream bridge.

At sites with no embankment to function as a weir or at sites where the tailwater drowns out the embankment, a composite bridge and road section was used to compute flow. Those sites were computed with friction-loss equations rather than with a bridge routine.

Total scour is taken as the sum of local scour plus contraction scour. If the model predicted negative contraction scour (aggradation), the contraction-scour value was assumed to be zero in determining the total scour depth (table 1). This assumption was made so that a negative contraction scour would not mask the potentially detrimental effects of local scour at a pier. No abutment scour evaluations were made in this study.

Table 1. Cumulative scour depths for the modeled discharges at structure I-69-76-4775 crossing Salamonie River in Huntington County, Indiana

Pier number ¹	Stationing from bridge plans ²	Initial bed- elevation at pier (feet)	Main- channel contrac- tion scour depth (feet)	Local scour depth (feet)	Worst- case total- scour depth ³ (feet)	Bottom elevation of pier (feet)	Worst- case bed elevation after scour ⁴ (feet)
**************************************	••••	Modeled	discharge ⁵ is 15,8	300 cubic feet	per second		
1	245+83	799	7.5	6.2	13.7	784.5	774.1
2	246+56	788	7.5	6.2	13.7	784.0	774.1
3	247+31	788	7.5	6.2	13.7	776.5	774.1
4	248+06	795	7.5	6.2	13.7	781.5	774.1
5	248+81	797	7.5	6.2	13.7	788.5	774.1
		Modeled	discharge is 26,9	00 cubic feet p	per second	,	
1	245+83	799	13.9	7.0	20.9	784.5	766.9
2	246+56	788	13.9	7.0	20.9	784.0	766.9
3	247+31	788	13.9	7.0	20.9	776.5	766.9
4	248+06	795	13.9	7.0	20.9	781.5	766.9
5	248+81	797	13.9	7.0	20.9	788.5	766.9

¹Pier numbers were assigned from left to right as shown on the bridge plans.

²Stationing is the center line of the pier as determined from the bridge plans. Stationing from bridge plan, 245+83, represents a point 24,583 feet from an arbitrary starting location referenced on the bridge plans.

³Worst-case total-scour depths are generated by summing the calculated contraction-scour depth with the worst case of local scour.

⁴Worst-case bed elevation is computed by subtracting the worst-case total-scour depth from the lowest initial bed elevation in the bridge opening (787.8 feet).

⁵Coordinated discharge.

SPECIAL CONSIDERATIONS

Model runs indicate the water-surface elevation at the bridge is lower than the low-steel elevation for the modeled discharges. Therefore, there should be no pressure flow through the bridge opening for the discharges modeled.

Salamonie Lake is immediately downstream from the I-69-76-4775 bridge. During periods of high flow, back-water effect created by the lake may reduce flow velocities near the bridge and thereby reduce the potential for scouring. The modelling described in this report, however, has been done without consideration of possible back-water effect from the lake.

RESULTS

Scour depths were computed with a version of WSPRO (Larry Arneson, Federal Highway Administration, written commun., 1996) modified from Shearman (1990). This version of WSPRO includes scour calculations in the model output. Scour depths were calculated assuming an infinite depth of material that could erode and a homogeneous particle-size distribution. The results of the scour analysis are presented in table 1; a complete input file and output results are presented in the appendix.

REFERENCES

- Hoggatt, R.E., 1975, Drainage areas of Indiana streams: U.S. Geological Survey, Water Resources Division, 231 p.
- Indiana State Highway Commission, 1962, Bridge plans Interstate Route 69: Bridge File I-69-76-4775.
- Lagasse, P.F.; Schall, J.D.; Johnson, F.; Richardson, E.V.; and Chang, F., 1995, Stream stability at highway structures (2d ed.): Federal Highway Administration, Hydraulic Engineering Circular No. 20, Publication FHWA-IP-90-014, 144 p.
- Richardson, E.V., and Davis, S.R., 1995, Evaluating scour at bridges (3d ed.): Federal Highway Administration, Hydraulic Engineering Circular No. 18, Publication FHWA-IP-90-017, 204 p.
- Shearman, J.O., 1990, User's manual for WSPRO, a computer model for water-surface profile computations: Federal Highway Administration Publication FHWA-IP-89-027, 177 p.

APPENDIX

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T1
          I-69 Over Salamonie River
                                             169-76-4775
          County: Huntington
Т2
                                             Ouad: Warren 75A
Т3
          11-08-96
                                             Bret A. Robinson
SI
          0
          15800 26900
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XS
     EXIT 0
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                     24531 820
                                24598 810 24604 810
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                                                                  24639 800
GR
          24678 790
                     24685 789
                                24707 788
                                           24847 788
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GR
          25648 800
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N
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         24932 0809.5 24932 0810.5
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 Minimum Y-Elevation: 788.000 (associated X-Station: 24847.000)
 Maximum Y-Elevation: 830.000 (associated X-Station: 23963.000)
                Roughness Data ( 3 SubAreas )
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  ********************* W S P R O ****************
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          Model for Water-Surface Profile Computations.
         Input Units: English / Output Units: English
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        I-69 OVER SALAMONIE RIVER
                                  I69-76-4775
      COUNTY: HUNTINGTON
                                QUAD: WARREN 75A
       11-08-96
                                 BRET A. ROBINSON
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              Data Summary For Header Record FULLV
              420. Cross-Section Skew: .0 Error Code
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            .00000 Averaging Conveyance By Geometric Mean.
Valley Slope:
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            797 9 4
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            797 12 5
  PD
            800 12 5
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  PD
            800 15 1
  CD
            3 230 2 811
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*** Completed Reading Data Associated With Header Record BRDGE ***
+++072 NOTICE: X-coordinate # 2 increased to eliminate vertical segment.
+++072 NOTICE: X-coordinate #17 increased to eliminate vertical segment.

*** Storing Bridge Data In Temporary File As Record Number 3 ***

*** Data Summary For Bridge Record BRDGE ***

SRD Location: 420. Cross-Section Skew: .0 Error Code 0

Valley Slope: ****** Averaging Conveyance By Geometric Mean.

Energy Loss Coefficients -> Expansion: .50 Contraction: .00

X,Y-coordinates (58 pairs)

x	Y	Х	Y	x	Y
24529.000	812.600	24529.100	811.800	24531.000	811.700
24567.000	797.100	24588.000	796.700	24600.000	791.000
24615.000	787.800	24700.000	787.700	24718.000	788.300
24755.000	787.600	24801.000	788.900	24810.000	796.500
24844.000	797.400	24901.000	796.900	24930.000	809.500
24932.000	809.500	24932.100	810.500	24923.000	810.500
24908.000	810.000	24895.000	809.000	24888.000	808.200
24882.000	807.500	24876.000	809.100	24864.000	810.400
24855.000	810.900	24844.000	811.000	24829.000	810.500
24817.000	809.400	24810.000	808.100	24807.000	807.100
24805.000	808.200	24798.000	809.600	24789.000	810.600
24777.000	811.300	24763.000	811.300	24753.000	810.900
24741.000	809.700	24735.000	808.700	24731.000	807.500
24728.000	808.700	24716.000	810.800	24705.000	811.600
24689.000	811.800	24676.000	811.300	24666.000	810.200
24660.000	809.000	24657.000	807.700	24651.000	809.600
24642.000	811.000	24628.000	811.900	24613.000	812.100
24599.000	811.400	24589.000	810.400	24582.000	808.900

```
24575.000
          809.800 24557.000 811.600 24542.000
24529.000 812.600
                     -----
              Minimum and Maximum X, Y-coordinates
 Minimum X-Station: 24529.000 (associated Y-Elevation: 812.600)
 Maximum X-Station: 24932.100 (associated Y-Elevation: 810.500)
 Minimum Y-Elevation: 787.600 (associated X-Station: 24755.000)
 Maximum Y-Elevation: 812.600 (associated X-Station: 24529.000)
                 Roughness Data ( 1 SubAreas )
                       Roughness Horizontal
               SubArea Coefficient Breakpoint
               ......
                          .034
               ..... ......... ......
               Discharge coefficient parameters
           BRType BRWdth EMBSS EMBElv UserCD
                 230.000 2.00 811.000 *******
             3
                  Pressure flow elevations
                     AVBCEL PFE1ev
                  ****** 810.000
                   Abutment Parameters
      ABSLPL ABSLPR XTOELT YTOELT XTOERT YTOERT
     ****** ***** ***** ****** ****** *****
               Pier/Pile Data ( 9 Group(s) )
             Code Indicates Bridge Uses Piers
            Group Elevation Gross Width Number
           ..... ...... ...... ......
                  788.000 3.000
788.100 3.000
788.100 6.000
796.000 6.000
              1
              2
              3
              4
                  796.000
797.000 9.000
797.000 12.000
12.000
              5
              6
              7
              8
                   800.000
                               15.000
           Finished Processing Header Record BRDGE
 ******************** W S P R O ***************
    Federal Highway Administration - U. S. Geological Survey
          Model for Water-Surface Profile Computations.
         Input Units: English / Output Units: English
```

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I-69 OVER SALAMONIE RIVER
                                      I69-76-4775
       COUNTY: HUNTINGTON
                                    QUAD: WARREN 75A
       11-08-96
                                    BRET A. ROBINSON
DC 0 BRDGE 24589 24809 24500 24730 * 15
        24529 24932 3 * * 1 1 1.1
DP
        24529 24932 3 * * 1 1 1.1
DP
        24529 24932 3 * * 1 1 1.1
        24529 24932 3 * * 1 1 1.1
DP
DP
        24529 24932 3 * * 1 1 1.1
             Starting To Process Header Record APPR
        *-----
XS
   APPR 1070
GR
        23865 830 24128 820 24249 810 24334 800 24501 800 24523 789
        24541 788 24712 788 24717 789 24729 797 24877 797 25502 800
GR
GR
        25583 810 25752 820 26069 830
        .100 .034 .035
N
        24500 24725
SA
    Completed Reading Data Associated With Header Record APPR
*** Storing X-Section Data In Temporary File As Record Number 4 ***
* * *
               Data Summary For Header Record APPR
                                                           ***
SRD Location:
               1070. Cross-Section Skew: .0 Error Code
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00
                  X,Y-coordinates (15 pairs)
             Y
                          Х
                                Y
                     -----
                                          ------
------
         -----
                                820.000
23865.000
           830.000
                     24128.000
                                           24249.000
                                                       810.000
                                          24523.000
24334.000
                                 800.000
           800.000
                     24501.000
                                                       789.000
            788.000 24712.000
24541.000
                                  788.000 24717.000
                                                        789.000
                                 797.000 25502.000
24729.000
           797.000 24877.000
                                                        800.000
                    25752.000 820.000 26069.000
25583.000 810.000
                                                        830.000
                      -----
                                           -----
              Minimum and Maximum X,Y-coordinates
 Minimum X-Station: 23865.000 (associated Y-Elevation: 830.000)
 Maximum X-Station: 26069.000 (associated Y-Elevation: 830.000)
 Minimum Y-Elevation: 788.000 (associated X-Station: 24712.000)
 Maximum Y-Elevation: 830.000 (associated X-Station: 23865.000)
                 Roughness Data ( 3 SubAreas )
                        Roughness Horizontal
               SubArea Coefficient Breakpoint
                -----
                       -----
                                  . . . . . . . . . .
                          .100
                          - - -
                  2
                          .034
                                   ******
                          - - -
                  3
                           .035
```

Bridge d	Bridge datum projection(s): XREFLT XREFRT FDSTLT FDSTRT								
	* * E			ng Header I					
	Federal Hig Mode Input	nhway Adm el for Wa : Units:	inistrat ter-Surf English	PRO *** ion - U. ace Profile / Output	S. Geologi Computati Units: Eng	cal Survey			
* EX		VER SALAM HUNTINGTO	ONIE RIV			75A	*		
	<pre>*=======* * Summary of Boundary Condition Information * *=======*</pre>								
#	Reach Discharge	E1		e Friction Slope	Flo	ow Regime			
1 2	15800.00	**	***** *****	.0004	Sul	o-Critical o-Critical			
	*	Beginnin	g 2 Pro	======== file Calcul ========	ation(s)	*			
	Federal Hig Mode Input	hway Admi l for Wa Units:	inistrat ter-Surf English	PRO *** ion - U. ace Profile / Output	S. Geologia Computation Units: Engl	cal Survey ons. lish			
*	* I-69 OVER SALAMONIE RIVER I69-76-4775 COUNTY: HUNTINGTON QUAD: WARREN 75A 11-08-96 BRET A. ROBINSON								
	-	WSEL EGEL CRWS	HF HO	Q V FR #	AREA K SF	SRDL FLEN ALPHA	LEW REW ERR		
Header '	: EXIT Type: XS .000	802.163 802.434	.271	15800.000 2.683	5889.287	*****	25692.340		
	: FULLV Type: FV			15800.000 2.600		420.000 420.000			

SRD: 420.000 794.173 .000 .301 .0004 2.451 -.001 << The Preceding Data Reflect The "Unconstricted" Profile >>> ===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID "APPR". KRATIO: 1.44 802.639 .125 15800.000 7043.511 650.000 24311.570 Section: APPR 802.765 .170 2.243 1174257.00 650.000 25523.380 Header Type: AS SRD: 1070.000 793.922 .000 .208 .0003 1.601 -.001 <<< The Preceding Data Reflect The "Unconstricted" Profile >>> <<< The Following Data Reflect The "Constricted" Profile >>> <<< Beginning Bridge/Culvert Hydraulic Computations >>> WSEL VHD 0 AREA SRDL LEW HF V K EGEL FLEN REW FR # SF CRWS но ALPHA ______ 802.284 .346 15800.000 3702.867 420.000 24554.220 Section: BRDGE Header Type: BR 802.630 .182 4.267 757370.40 420.000 24913.390 SRD: 420.000 793.921 .014 .259 ****** 1.221 -.002 Specific Bridge Information C P/A PFELEV BLEN XLAB Bridge Type 3 Flow Type 1 ----- ----- -----.9051 .034 810.000 ****** ***** ***** Pier/Pile Code 0 Q V WSEL VHD AREA SRDL EGEL HF K FLEN REW но FR # SF ALPHA CRWS Section: APPR 802.754 .120 15800.000 7182.569 420.000 24310.590 Header Type: AS 802.874 .129 2.200 1203000.00 455.521 25524.310 SRD: 1070.000 793.922 .115 201 2022 Approach Section APPR Flow Contraction Information M(G) M(K) KQ XLKQ XRKQ OTEL259 889476.8 ******* ****** 802.754 <<< End of Bridge Hydraulics Computations >>> ******************** W S P R O **************** Federal Highway Administration - U. S. Geological Survey Model for Water-Surface Profile Computations. Input Units: English / Output Units: English *-----I-69 OVER SALAMONIE RIVER I69-76-4775

-16-

COUNTY: HUNTINGTON

QUAD: WARREN 75A

11-08-96

BRET A. ROBINSON

	WSEL EGEL CRWS	VHD HF HO	Q V FR #	AREA K SF	SRDL FLEN ALPHA	LEW REW ERR
Section: EXIT Header Type: XS SRD: .000	805.645 805.969 796.641		26900.000 2.762 .276	9738.156 1344589.00 *****	****** ****** 2.732	
Section: FULLV Header Type: FV SRD: 420.000	805.821 806.133 796.641	.312 .164 .000	26900.000 2.706 .269	9939.874 1377104.00 .0004	· -	24615.700 25767.320 001

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID "APPR". KRATIO: 1.61

Section: APPR	806.161	.125	26900.000	11413.640	650.000 24	281.630
Header Type: AS	806.286	.154	2.357	2222243.00	650.000.25	551.900
SRD: 1070.000	796.346	.000	.167	.0002	1.448	.000

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

<<< The Following Data Reflect The "Constricted" Profile >>> <<< Beginning Bridge/Culvert Hydraulic Computations >>>

	WSEL EGEL CRWS	VHD HF HO	v	AREA K SF	FLEN	
Section: BRDGE Header Type: BR SRD: 420.000		.198	5.449	4937.100 1186017.00 *****	420.000	24921.130
Specific Bridge Bridge Type 3 Pier/Pile Code	Flow Type 1				* *****	·
	WSEL EGEL CRWS		V	AREA K SF		
Section: APPR Header Type: AS SRD: 1070.000	806.571	.129				25554.280
				craction Info		

.704 .425 1336569.0 ******* ****** 806.455

<<< End of Bridge Hydraulics	s Computations >>>
*************************** W S P R O * Federal Highway Administration - U Model for Water-Surface Profi Input Units: English / Outpu	J. S. Geological Survey le Computations. It Units: English
I-69 OVER SALAMONIE RIVER COUNTY: HUNTINGTON	
*** Live-Bed Contraction Scour Calculation	ons for Header Record BRDGE ***
Constants and Input Va	riables
*	
Bed Material Transport Mode Fa Total Pier Width Value *	(Pw): 15.000
# Depth Contract Approach Contract Approach 7.499 15745.760 10289.150 205.000 230 Approach Channel Depth: 13.730 . 2 13.906 24615.050 13473.330 205.000 230 Approach Channel Depth: 17.431	0.000 Left: ****** *****************************
*	*
	I69-76-4775 QUAD: WARREN 75A BRET A. ROBINSON
*** Pier Scour Calculations for He	ader Record BRDGE ***
Constants and Input Va	riables
Pier Width: 3.00	
Bed Material Factor Velocity Multiplier	(K1): 1.00
*	*

#	Depth	Loca Flow	WSE	Depth	Velocity	Froude #	Left	Right
1	6.21 7.04	15800.000 26900.000	802.399 805.778	14.799 18.178	5.175 6.492	.237 .268	24529.000 24529.000	24932.000 24932.000
	Fed	Input Un	y Admini or Water its: Eng	stration -Surface lish /	n - U. e Profile Output	S. Geolog Computat Units: En	ical Surve ions. glish	У
	I-69 OVER SALAMONIE RIVER COUNTY: HUNTINGTON 11-08-96			I69-76-4775 QUAD: WARREN 75A BRET A. ROBINSON				
	*** Pier Scour Calculations for Header Record BRDGE *** Constants and Input Variables Pier Width: 3.000							
		Pier S Flow A Bed Co Bed Ma Veloci Depth	hape Fac ngle of ndition terial F ty Multi Multipli	tor Attack 1 Factor actor plier er	() Factor () () ()	K1): 1. K2): 1. K3): 1. K4): 1. VM): 1.	00 00 10 00 00	
#	Depth	Loca Flow	WSE	Depth	Velocity	Froude #	Left	Right
1 2	6.21 7.04	15800.000 26900.000	802.399 805.778	14.799 18.178	5.175 6.492	.237 .268	24529.000 24529.000	24932.000 24932.000

	Constants and Input Variables							

Pier Width: 3.000

		*						*		
		Pier S	Shape Fac	tor		(K1):	1.0	00		
	Flow Angle of Attack Factor Bed Condition Factor Bed Material Factor Velocity Multiplier				actor	(K2): 1.00				
		Bed Co	ndition	Factor		(K3):	1.3	10		
		Bed Ma	terial F	actor		(K4):	1.0	00		
		Veloci	ty Multi	plier		(VM):	1.0	00		
		Depth	Multipli	er		(YM):	1.0	00		
		*						*		
	G =====	T	.1.4	a	D			V 0-		
#	Scour	Loca Flow	.11zed Hy	Donth	Volcait	ies	 #	X-St	ations	
11										
1	6.21	15800.000	802.399	14.799	5.175	• :	237	24529.000	24932.000	
2	7.04	26900.000	805.778	18.178	6.492		268	24529.000	24932.000	
	-						- -			
								•		

	Fed	eral Highwa	_						У	
			or Water its: Eng			_				
	*	Input on							-	
		T-69 OVER	SALAMONT	E RIVER		T69-76	5-477	75		
	c	COUNTY: HUNTINGTON					QUAD: WARREN 75A BRET A. ROBINSON			
	1									
	**	* Pier Sco	ur Calcu	lations	for Head	der Red	cord	BRDGE **	*	
			Constant	s and In	put Var	iables				
			Pier		3.000					
			hape Fac							
			nape rac	ot Attack F	actor	(K2) •	1.0) ()) ()		
		Flow A	nale of i	ACCUCK I				, 0		
		Flow A	ngle of A	Factor		(K3):	1.1	.0		
		Flow A Bed Co	ngle of A ndition 1 terial Fa	Factor		(K3):	1.1	.0		
		Flow A Bed Co Bed Ma	ndition 1 terial Fa	Factor actor		(K3): (K4):	1.1	LO DO		
		Flow A Bed Co Bed Ma Veloci	ndition 1	Factor actor plier		(K3): (K4): (VM):	1.1 1.0	LO 00 00		
		Flow A Bed Co Bed Ma Veloci Depth	ndition l terial Fa ty Multip	Factor actor plier er		(K3): (K4): (VM): (YM):	1.1 1.0 1.0	10 00 00 00		
		Flow A Bed Co Bed Ma Veloci Depth	ndition laterial Faty Multiplie	Factor actor plier er		(K3): (K4): (VM): (YM):	1.1 1.0 1.0	10 00 00 00 00		
u	Scour	Flow A Bed Co Bed Ma Veloci Depth *	ndition laterial Faty Multiplic	Factor actor plier er draulic	Propert:	(K3): (K4): (VM): (YM):	1.0	10 00 00 00 * X-St	ations	
#	Depth	Flow A Bed Co Bed Ma Veloci Depth * Loca Flow	ndition laterial Faty Multiplic Lized Hydroxe WSE	Factor actor plier er draulic Depth	Propert: Velocity	(K3): (K4): (VM): (YM): ies	1.1 1.0 1.0 1.0	10 00 00 00 * X-St Left	Right	
	Depth	Flow A Bed Co Bed Ma Veloci Depth * Loca Flow	ndition I terial Fa ty Multip Multiplic lized Hyd WSE	Factor actor plier er draulic Depth	Propert: Velocity	(K3): (K4): (VM): (YM): ies	1.1 1.0 1.0 1.0	10 00 00 00 * X-St Left	Right	
1	Depth 6.21	Flow A Bed Co Bed Ma Veloci Depth * Loca Flow 15800.000	ndition I terial Fa ty Multip Multiplio lized Hyo WSE 802.399	Factor actor plier er draulic Depth 14.799	Propert: Velocity	(K3): (K4): (VM): (YM): ies	1.1 1.0 1.0 1.0 	10 00 00 * X-St Left 	Right24932.000	
1	Depth 6.21 7.04	Flow A Bed Co Bed Ma Veloci Depth * Loca Flow	ndition I terial Fa ty Multip Multiplic Sized Hyd WSE 802.399 805.778	Factor actor plier plier draulic Depth 14.799 18.178	Propert: Velocity 5.175 6.492	(K3): (K4): (VM): (YM): ies	1.1 1.0 1.0 1.0 1.0 1.0 1.0 2.7 2.7 2.68	10 00 00 00 * X-St Left 24529.000 24529.000	Right 24932.000 24932.000	
1 2	Depth 6.21 7.04	Flow A Bed Co Bed Ma Veloci Depth *Loca Flow15800.000 26900.000	ndition I terial Fa ty Multip Multiplic Sized Hyd WSE 802.399 805.778	Factor actor plier plier draulic Depth 14.799 18.178	Propert: Velocity 5.175 6.492	(K3): (K4): (VM): (YM): ies	1.1 1.0 1.0 1.0 1.0 1.0 1.0 2.7 2.7 2.68	10 00 00 00 * X-St Left 24529.000 24529.000	Right 24932.000 24932.000	
1 2	Depth 6.21 7.04	Flow A Bed Co Bed Ma Veloci Depth * Loca Flow 15800.000 26900.000	ndition I terial Fa ty Multip Multiplication lized Hyd WSE 802.399 805.778	Factor actor olier olier or olier ol	Propertive Velocity 5.175 6.492	(K3): (K4): (VM): (YM): ies y Frouc	1.1 1.0 1.0 1.0 1.0 1.0 2.7 2.6 2.37	10 00 00 * X-St Left 24529.000 24529.000	Right 24932.000 24932.000	
1 2	Depth 6.21 7.04	Flow A Bed Co Bed Ma Veloci Depth *Loca Flow15800.000 26900.000	ndition I terial Fa ty Multip Multiplication lized Hyd WSE 802.399 805.778	Factor actor olier olier or olier ol	Propertive Velocity 5.175 6.492	(K3): (K4): (VM): (YM): ies y Frouc	1.1 1.0 1.0 1.0 1.0 1.0 2.7 2.6 2.37	10 00 00 * X-St Left 24529.000 24529.000	Right 24932.000 24932.000	
1 2	Depth 6.21 7.04	Flow A Bed Co Bed Ma Veloci Depth * Loca Flow 15800.000 26900.000	ndition laterial Faty Multiplication laterial Faty Multiplication laterial Hydrox WSE	Factor actor plier plier draulic Depth 14.799 18.178 W S P	Propert: Velocity 5.175 6.492	(K3): (K4): (VM): (YM): ies y Frouc ******	1.1 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	10 00 00 00 * X-St Left 24529.000 24529.000	Right 24932.000 24932.000	
1 2	Depth 6.21 7.04	Flow A Bed Co Bed Ma Veloci Depth * Loca Flow 15800.000 26900.000 **************************	ndition I terial Fa ty Multip Multiplic lized Hyo WSE 802.399 805.778 ******** y Adminis	Factor actor actor plier plier ar draulic Depth 14.799 18.178 W S P stration Surface	Propert: Velocity 5.175 6.492 R O ***	(K3): (K4): (VM): (YM): ies y Frouc ****** S. Gec e Compu	1.1 1.0 1.0 1.0 1.0 1.0 1e # 237 268	10 00 00 00 * X-St Left 24529.000 24529.000 	Right 24932.000 24932.000	
1 2	Depth 6.21 7.04 *****	Flow A Bed Co Bed Ma Veloci Depth * Loca Flow 15800.000 26900.000 *********** eral Highwa Model f Input Un	ndition I terial Fa ty Multip Multiplication lized Hyd WSE 802.399 805.778 ******* y Adminis or Water its: Engi	Factor actor actor plier plier ar draulic Depth 14.799 18.178 W S P stration Surface lish /	Propert: Velocity 5.175 6.492 R O *** Profile Output	(K3): (K4): (VM): (YM): ies y Frouc ****** S. Geo e Compu	1.1 1.0 1.0 1.0 1.0 1.0 1e # 237 268	10 00 00 00 * X-St Left 24529.000 24529.000 	Right 24932.000 24932.000	
1 2	Depth 6.21 7.04 *****	Flow A Bed Co Bed Ma Veloci Depth * Loca Flow 15800.000 26900.000 **************************	ndition I terial Fa ty Multip Multiplication lized Hyd WSE 802.399 805.778 ******* y Administor Water its: Engine	Factor actor actor plier er draulic Depth 14.799 18.178 W S P stration Surface lish /	Propert: Velocity 5.175 6.492 R O *** - U. Profile Output	(K3): (K4): (VM): (YM): ies y Frouc ****** S. Gec e Compu	1.1 1.0 1.0 1.0 1.0 1.0 1e # 237 268 	10 00 00 00 * X-St Left 24529.000 24529.000 	Right 24932.000 24932.000	

COUNTY: HUNTINGTON QUAD: WARREN 75A 11-08-96 BRET A. ROBINSON

*** Pier Scour Calculations for Header Record BRDGE ***

Constants and Input Variables

Pier Width: 3.00	0	_
Pier Shape Factor	(K1):	1.00
Flow Angle of Attack Factor	(K2):	1.00
Bed Condition Factor	(K3):	1.10
Bed Material Factor	(K4):	1.00
Velocity Multiplier	(VM):	1.00
Depth Multiplier	(YM):	1.00

Scour --- Localized Hydraulic Properties --- X-Stations -# Depth Flow WSE Depth Velocity Froude # Left Right

1 6.21 15800.000 802.399 14.799 5.175 .237 24529.000 24932.000
2 7.04 26900.000 805.778 18.178 6.492 .268 24529.000 24932.000

ER